# Computational real algebraic geometry and applications to robotics

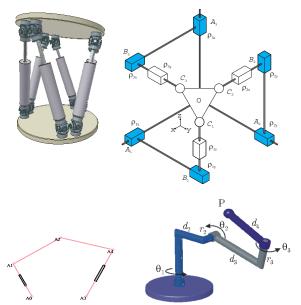
JNCF lecture, part 1

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March 1st, 2021

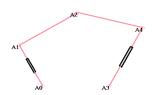
#### Mechanisms



### Modeling

- Joint variables
  - $\bullet$   $r_1, r_2$
- Pose variables
  - X, Y
- Passive variables
  - $\theta_1, \theta_2$



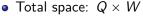


Equations

$$(F) \left\{ \begin{array}{l} \mathbf{x} = \cos(\frac{2\pi}{3})r_1 + \cos(\theta_1) \\ \mathbf{x} = 1 + \cos(\frac{\pi}{3})r_2 + \cos(\theta_2) \\ \mathbf{y} = \sin(\frac{2\pi}{3})r_1 + \sin(\theta_1) \\ \mathbf{y} = 1 + \sin(\frac{\pi}{3})r_2 + \sin(\theta_2) \end{array} \right.$$

### Workspace, Joint space

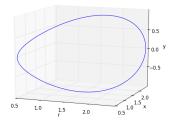
- Q: joint space
- W: workspace



• solutions of F:  $V(F) \subset W \times Q$ 



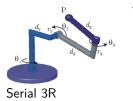
Parallel RPR-R

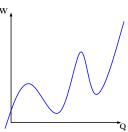


- Canonical projections:
  - $\pi_W:V(F)\to W$
  - $\pi_O: V(F) \to W$

#### Serial robot

- Glossary:
  - P: prismatic joint
  - R: rotation joint
  - U: Cardan joint
  - S: spherical joint



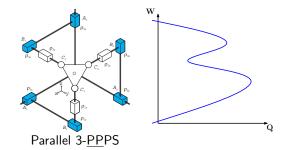


#### **Properties**

- Inverse Kinematics (IK) hard
- Forward Kinematics (FK) easy: 1 solutions

#### Parallel robot

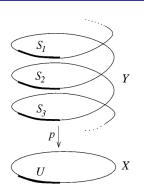
- Glossary:
  - P: prismatic joint
  - R: rotation joint
  - U: Cardan joint
  - S: spherical joint



#### **Properties**

- Inverse Kinemaics (IK) easy
- Forward Kinematics (FK) hard: several solutions
- 2 solutions can cross
  - loose of control
  - break

### Covering map



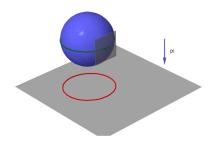
#### **Definition**

The continuous map  $f: S \rightarrow U$  is a covering map if:

$$f^{-1}(U) = S_1 \cup \cdots \cup S_k$$
 where 
$$\begin{cases} S_i \stackrel{f}{\simeq} U \\ S_i \text{ pairwise disjoint.} \end{cases}$$

### Critical points

- $V \subset \mathbb{R}^n$  smooth variety of dimension p
- $\bullet$   $\pi:V \to \mathbb{R}^p$  canonical projection



#### Critical points

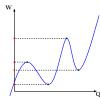
Let T(a) be the linear space tangent to V at point a. The critical points a of V for the projection  $\pi$  satisfy:

$$dim(\pi(T(a))) < p$$

#### Case of the serial robot

Hypothesis: V(F) smooth, bounded, equidimensional.

- FK: always 1 solution  $\Rightarrow \pi_Q : V(F) \to Q$  invertible
- IK: partition W in  $W_0, W_1, \ldots, W_k$  s.t.:
  - ullet  $W_0$  are the critical values of  $\pi_W$
  - $W_1, \ldots, W_k$  are the connected components of  $W \backslash W_0$
- Critical points of  $\pi_W$ : serial singularities



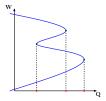
#### Theorem (covering map and critical values)

For all  $1 \le i \le k$ , the restriction of  $\pi_W$  to  $\pi_W^{-1}(W_i)$  is a covering map above  $W_i$ .

### Case of parallel robot

Hypothesis: V(F) smooth, bounded, equidimensional.

- IK: always 1 solution  $\Rightarrow \pi_W : V(F) \to W$  invertible
- FK: partition Q in  $Q_0, Q_1, \ldots, Q_k$  s.t.:
  - ullet  $Q_0$  are the critical values of  $\pi_Q$
  - ullet  $Q_1,\ldots,Q_k$  are the connected components of  $Qackslash Q_0$
- Critical points of  $\pi_Q$ : parallel singularities



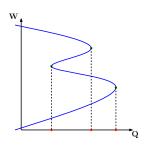
#### Theorem (covering map and critical values)

For all  $1 \le i \le k$ , the restriction of  $\pi_Q$  to  $\pi_Q^{-1}(Q_i)$  is a covering map above  $Q_i$ .

#### **Properties**

#### Case of parallel robots

- FK:  $F_q(x) = 0$ , system parametrized by q
- For fixed q, finitely many solutions (0-dimensional)
- $\pi_Q$  is not a covering map near q
  - ⇒ two sheets of solutions cross
  - $\Rightarrow F_q(x) = 0$  has singular solutions



#### • Remark: V(F)

- not bounded: take asymptotes into account
- not smooth: take singularities into account

### Computation

Hypothesis: V(F) smooth, bounded, equidimensional.

$$\underbrace{\frac{\partial F}{\partial q}}_{A} dq + \underbrace{\frac{\partial F}{\partial x}}_{B} dx = 0$$

Serial singularities

$$(S_s): F = 0, det(A) = 0$$

- $W_0$ , critical values of  $\pi_W$ : projection on  $x_i$  of solutions of  $(S_s)$
- $W_1, \ldots, W_k$ , complement of critical values

### Computation

Hypothesis: V(F) smooth, bounded, equidimensional.

$$\underbrace{\frac{\partial F}{\partial q}}_{A} dq + \underbrace{\frac{\partial F}{\partial x}}_{B} dx = 0$$

Parallel singularities

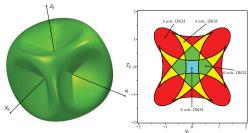
$$(S_p): F=0, det(B)=0$$

- $Q_0$ , critical values of  $\pi_Q$ : projection on  $q_i$  of solutions of  $(S_p)$
- $Q_1, \ldots, Q_k$ , complement of critical values

#### Example

- 3-PPPS:
  - Parallel
  - Joint variables:  $x_1, y_1, y_2, z_2, x_3, z_3$
  - Pose variables:  $p_x, p_y, p_z, \varphi, \theta, \sigma$

ullet Critical values of  $\pi_Q$ , and partition of Q

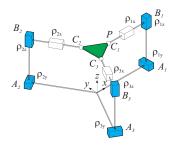


### Design challenges

- $E \subset W$  given shape
  - Design a parallel robot without singularities in E

$$\pi_W$$
(critical points of  $\pi_Q$ )  $\cap E = \emptyset$ 

- Maximise the volume of E (lecture P. Lairez)
- → design variables



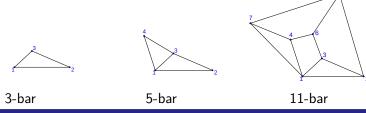
#### Demo

# Demo

#### Modeling equations

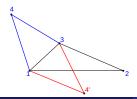
- Linkages
- Rotations 3D
- Singularities

### Planar Rigid Linkage: Laman Graph



#### Constraints

- Fixed length bars: cij
- Free revolute joints
- Zero degree of freedom

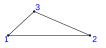


- Several assembly modes
- Number depends on c<sub>ij</sub>
- Max number of assembly modes?

Construction steps



• 3-bar rigid linkage

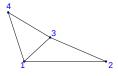


Construction steps



Henneberg steps:  $H_1$  and  $H_2$ 

• 5-bar rigid linkage

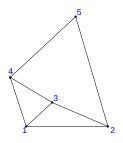


Construction steps



Henneberg steps:  $H_1$  and  $H_2$ 

• 7-bar rigid linkage

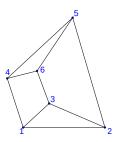


Construction steps



Henneberg steps:  $H_1$  and  $H_2$ 

• 9-bar rigid linkage

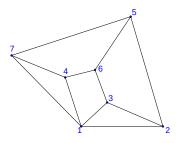


Construction steps



Henneberg steps:  $H_1$  and  $H_2$ 

• 11-bar rigid linkage



### Known properties

#### Theorem

A linkage is rigid  $\Leftrightarrow$  It can be constructed with  $H_1$  and  $H_2$ 

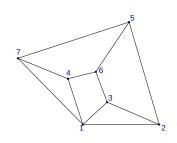
#### Corollary

$$\#Links = 2\#Joints - 3$$

### Algebraic Modeling I

- c<sub>ii</sub>: 10 parameters
- $x_i, y_i$ : 14 variables

$$\begin{cases} x_1 = 0, y_1 = 0 \\ x_2 = 1, y_2 = 0 \end{cases}$$

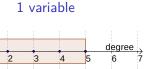


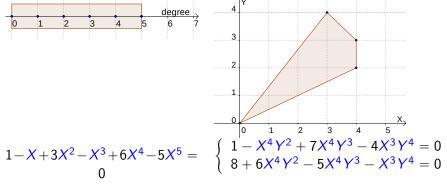
$$\begin{cases} x_3^2 + y_3^2 &= c_{13} \\ (x_3 - 1)^2 + y_3^2 &= c_{23} \\ (x_5 - 1)^2 + y_5^2 &= c_{25} \\ (x_6 - x_3)^2 + (y_6 - y_3)^2 &= c_{36} \\ x_4^2 + y_4^2 &= c_{14} \end{cases}$$

$$\begin{cases} x_3^2 + y_3^2 &= c_{13} \\ (x_3 - 1)^2 + y_3^2 &= c_{23} \\ (x_5 - 1)^2 + y_5^2 &= c_{25} \\ (x_6 - x_3)^2 + (y_6 - y_3)^2 &= c_{36} \\ x_4^2 + y_4^2 &= c_{14} \end{cases} \begin{cases} x_7^2 + y_7^2 &= c_{17} \\ (x_6 - x_4)^2 + (y_6 - y_4)^2 &= c_{46} \\ (x_5 - x_6)^2 + (y_5 - y_6)^2 &= c_{56} \\ (x_7 - x_5)^2 + (y_7 - y_5)^2 &= c_{57} \\ (x_4 - x_7)^2 + (y_4 - y_7)^2 &= c_{47} \end{cases}$$

#### Number of solutions

Mixed Volume: n! Volume(Support) (same support)





$$1 - X + 3X^2 - X^3 + 6X^4 - 5X^5 = 0$$

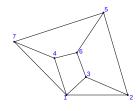
$$\begin{cases} 1 - X^4 Y^2 + 7X^4 Y^3 - 4X^3 Y^4 = 0 \\ 8 + 6X^4 Y^2 - 5X^4 Y^3 - X^3 Y^4 = 0 \end{cases}$$

• Our system: 2<sup>10</sup>

### Algebraic Modeling II

Cayley-Menger matrix or distance matrix

		$v_1$	<i>V</i> <sub>2</sub>	<i>V</i> 3	<i>V</i> 4	<i>V</i> 5	<i>v</i> <sub>6</sub>	<i>V</i> 7	
	Γ0	1	1	1	1	1	1	1	٦
$v_1$	1	0	<i>c</i> <sub>12</sub>	<i>c</i> <sub>13</sub>	<i>c</i> <sub>14</sub>	X <sub>15</sub>	<i>X</i> <sub>16</sub>	<i>c</i> <sub>17</sub>	
<i>v</i> <sub>2</sub>	1	<i>c</i> <sub>12</sub>	0	<i>C</i> <sub>23</sub>	X <sub>24</sub>	<i>C</i> <sub>25</sub>	<i>X</i> 26	X27	l
<i>V</i> 3	1	<i>c</i> <sub>13</sub>	<i>c</i> <sub>23</sub>	0	<i>X</i> 34	<i>X</i> 35	<i>C</i> <sub>36</sub>	<i>X</i> 37	-
<i>V</i> 4	1	<i>C</i> <sub>14</sub>	X <sub>24</sub>	<i>X</i> 34	0	<i>X</i> 45	C <sub>46</sub>	C47	١
<i>V</i> <sub>5</sub>	1	<i>X</i> <sub>15</sub>	<i>C</i> <sub>25</sub>	<i>X</i> 35	<i>X</i> 45	0	<i>C</i> 56	<i>C</i> 57	١
<i>v</i> <sub>6</sub>	1	<i>x</i> <sub>16</sub>	<i>X</i> <sub>26</sub>		<i>c</i> <sub>46</sub>		0	<i>x</i> <sub>67</sub>	١
<i>v</i> <sub>7</sub>		<i>c</i> <sub>17</sub>	<i>X</i> <sub>27</sub>	<i>X</i> 37	C <sub>47</sub>	<i>C</i> <sub>57</sub>	<i>X</i> 67	0	



#### Theorem

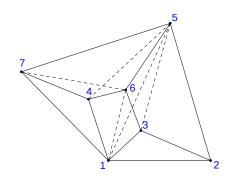
The distance matrix has rank 4.

### Corollary

All the 5x5 minors vanish.

### Algebraic Modeling II

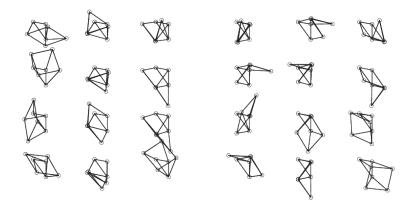
$$\begin{array}{lll} \left( \begin{array}{l} D(0,4,5,6,7)(c_{46},c_{47},c_{56},c_{57},x_{45},x_{67}) & = & 0 \\ D(0,1,4,6,7)(c_{14},c_{17},c_{46},c_{47},x_{16},x_{67}) & = & 0 \\ D(0,1,4,5,7)(c_{14},c_{17},c_{47},c_{57},x_{15},x_{45}) & = & 0 \\ D(0,1,2,3,5)(c_{12},c_{13},c_{25},c_{23},x_{15},x_{35}) & = & 0 \\ D(0,1,3,5,6)(c_{13},c_{36},c_{56},x_{15},x_{16},x_{35}) & = & 0 \end{array} \right)$$



- Upper bound
  - Mixed volume: 56
- Lower Bound?

### Sampling





### Number of assembly modes

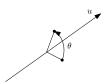
#### Maximal number of assembly modes

bars	3	5	7	9	11	13	15	17
upper	2	4	8	24	56	136	344	880
lower	2	4	8	24	56	136	344	860

- [Bartzosa, Emiris, Legerský, Tsigaridas 2021]
- Started in 2002 with Borcea
- Bartzosa, Borcea, Emiris, Legerský, M., Streinu, Capco, Gallet, Grasegger, Koutschan, Lubbes, Schicho, Tsigaridas, . . .

#### Rotations matrix in 3D

$$R = \begin{pmatrix} x_1 & x_2 & x_3 \\ y_1 & y_2 & y_3 \\ z_1 & z_2 & z_3 \end{pmatrix}$$



$$R^TR = I$$

- Action of R is a rotation by  $\theta$  around an axe u
- Set of rotation has dim 3

#### Euler matrix

$$R_{x}(\theta) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & \sin(\theta) \\ 0 & -\sin(\theta) & \cos(\theta) \end{pmatrix}$$

$$R_{y}(\varphi) = \begin{pmatrix} \cos(\varphi) & 0 & \sin(\varphi) \\ 0 & 1 & 0 \\ -\sin(\varphi) & 0 & \cos(\varphi) \end{pmatrix}$$

$$R_{\mathbf{z}}(\psi) = \begin{pmatrix} \cos(\psi) & \sin(\psi) & 0 \\ -\sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$R = R_z(\psi)R_v(\varphi)R_x(\theta)$$
 or  $R = R_z(\psi)R_v(\varphi)R_z(\theta)$ 

#### Quaternions matrix

$$q_i^2 + q_j^2 + q_k^2 + q_r^2 = 1$$

$$R = \begin{pmatrix} 1 - 2(q_j^2 + q_k^2) & 2(q_iq_j - q_kq_r) & 2(q_iq_k + q_jq_r) \\ 2(q_iq_j + q_kq_r) & 1 - 2(q_i^2 + q_k^2) & 2(q_jq_k - q_iq_r) \\ 2(q_iq_k - q_jq_r) & 2(q_jq_k + q_iq_r) & 1 - 2(q_i^2 + q_j^2) \end{pmatrix}$$

Rotation of axe:  $(q_i, q_i, q_k)$ angle:  $2 \arccos(q_r)$ 

### Anti-symmetric matrix - Exponential map

In 2D

$$\theta \Rightarrow \begin{pmatrix} \cos(\theta) & -\sin(\theta) \\ \sin(\theta) & \cos(\theta) \end{pmatrix}$$

In 3D

$$A = \begin{pmatrix} 0 & z & -y \\ -z & 0 & x \\ y & -x & 0 \end{pmatrix}$$

$$R = e^A$$

Rotation of axe: (x, y, z)angle:  $\|(x, y, z)\|_2$ 

### Anti-symmetric matrix - Cayley transform

In 2D

$$t = \tan\left(\frac{\theta}{2}\right) \Rightarrow \begin{pmatrix} \frac{1-t^2}{1+t^2} & \frac{-2t}{1+t^2}\\ \frac{2t}{1+t^2} & \frac{1-t^2}{1+t^2} \end{pmatrix}$$

In 3D

$$A = \begin{pmatrix} 0 & z & -y \\ -z & 0 & x \\ y & -x & 0 \end{pmatrix}$$

$$R = (I - A)(I + A)^{-1}$$

Rotation of axe: (x, y, z)

angle:  $2 \arctan(\|(x, y, z)\|_2)$ 

#### Plücker coordinates



How many lines intersect 4 given lines?

#### Plücker coordinates

$$P_{1} = \begin{pmatrix} x_{1} \\ y_{1} \\ z_{1} \end{pmatrix} \quad P_{2} = \begin{pmatrix} x_{2} \\ y_{2} \\ z_{2} \end{pmatrix} \quad M = \begin{pmatrix} x_{1} & x_{2} \\ y_{1} & y_{2} \\ z_{1} & z_{2} \\ 1 & 1 \end{pmatrix}$$

#### Definition

The Plücker coordinates of the line  $(P_1P_2)$  are the 6 minors of M

$$(d_x, d_y, d_z, m_x, m_y, m_z) = (P_2 - P_1, OP_1 \times OP_2)$$

•  $(d, m) \in \mathbf{P}_5$  is on the Klein quadric

$$d \cdot m = 0$$

• Lines (d, m) and (d', m') intersect implies

$$d \cdot m' + m \cdot d' = 0$$

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#### Plücker coordinates



0,1,2 or infinitely many lines cross the 4 given lines

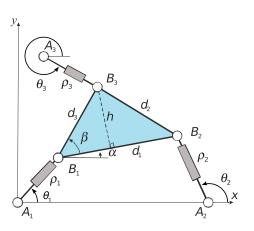
### Singularity modeling

$$f_1(q,x),\ldots,f_m(q,x)$$

$$B = \begin{array}{c} \frac{\partial}{\partial x_1} \cdots \frac{\partial}{\partial x_m} \\ \vdots \\ f_m \end{array} \left( \begin{array}{c} \frac{\partial f_i}{\partial x_j} \\ \end{array} \right)$$

- det(B) multi-linear in its columns/rows
- det(B) of deg 1 in  $x_j$  leads to a parametrization of the singularities
- Simplifies the analysis of the singularities, as in the 3-RPR [Coste 2012]

### Plan parallel robot 3-RPR

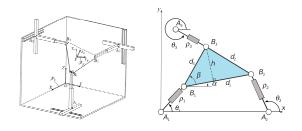


- 3 degrees of freedom
- $d_1, d_2, d_3, A_1, A_2, A_3$  fixed
- Joint variables:  $r_1, r_2, r_3$
- Pose variables:  $\alpha, B_{1x}, B_{1y}$

#### Demo

# Demo

### Singularity of parallel manipulator with Plücker vectors



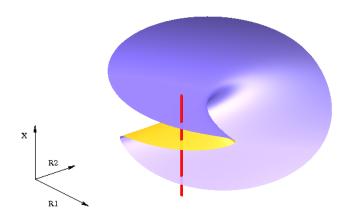
#### Remark

If the leg-platorm joints are spherical, the rows of the inverse kinematic Jacobian matrix  $A^{-1}B$  will involve the Plücker coordinates of lines associated to the legs.

⇒ singularities can be interpreted geometrically

### Cuspidal configuration

- Cuspidal point: point of order  $\geqslant 3$
- Characterization: A cuspidal robot has at least one cuspidal point



#### Demo

# Demo

### Further reading





# À suivre

### Solving systems

- With initial point
  - Newton
- Without initial point
  - Symbolic approaches
  - Numerical approaches