# Size-varying respiratory aerosols modeling

Amina Mecherbet and Frédérique Noel

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Advisors:

Laurent Boudin, Céline Grandmont, Bérénice Grec and Sébastien Martin.

### Introduction

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### Introduction

#### Purpose

- Modeling of particles (aerosol) motion in the lung.
- Understanding aerosol deposition maps on bronchi walls.
- Influence of the radius growth (water vapor exchange) on the aerosol deposition.

#### Previous model

Fluid particle model : L. Boudin, C. Grandmont, A. Lorz and A. Moussa, Modelling and Numerics for Respiratory Aerosols (2015). Model assumptions :

- The aerosol volume fraction in the mixture remains negligible.
- No interaction between particles.
- Aerosol can have an effect on the fluid (Retroaction effect).

# Model description

We denote by  $\Omega$  the fluid domain, which is a cylinder or a branch and is assumed to be fix in time.



**FIGURE** – Domain

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Image: A matrix

### Fluid equations

(u, p) represents the fluid velocity and its pressure satisfying a Navier-Stokes equation :

$$\left(\begin{array}{ccc} \rho_{\mathsf{air}}[\partial_t u + (u \cdot \nabla) u] - \eta \Delta u + \nabla p &=& \mathsf{F}, \\ \operatorname{div}(u) = \mathbf{0}, & & \operatorname{on} \, \mathbb{R}^+ \times \Omega, \end{array}\right.$$

completed with the following boundary and initial conditions :

$$\left(\begin{array}{cccc}
u &=& u^{\text{in}}, \text{ on } \Gamma^{\text{in}}, \\
u &=& 0, \text{ on } \Gamma^{\text{wall}}, \\
\sigma(u,p) \cdot n &=& 0, \text{ on } \Gamma^{\text{out}}, \\
u(0,\cdot) &=& u_0, \text{ on } \Omega,
\end{array}\right)$$

where  $\sigma(u, p)$  is the stress tensor and *F* is the particles retroaction term defined as follows :

$$\alpha = \frac{6\pi\eta r}{m},$$
  

$$F = -\int m\alpha(u-v)fdv.$$

### **Density equation**

For all  $t \in \mathbb{R}^+$ ,  $x \in \Omega$  and  $v \in \mathbb{R}^3$ , f(t, x, v) represents the number of droplets located in the elementary volume of the domain, at time *t*, position *x* and velocity *v*. The density *f* satisfies the following equation :

$$\partial_t f + \mathbf{v} \cdot \nabla_x f + \operatorname{div}_{\mathbf{v}}(\alpha(\mathbf{u} - \mathbf{v})f) = 0, \text{ on } \mathbb{R}^+ \times \Omega \times \mathbb{R}^3,$$

completed with the following initial and boundary conditions :

$$\left\{ \begin{array}{rll} f &=& 0, \text{ on } \Gamma^{\mathsf{wall}} \times \mathbb{R}^3, \text{ if } \boldsymbol{v} \cdot \boldsymbol{n} \leq 0, \\ f_{|t=0} &=& f_{\mathsf{init}}, \text{ on } \Omega \times \mathbb{R}^3. \end{array} \right.$$

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# Radius growth and temperature variation

**ODE System :** We denote by  $T_d$  the droplet temperature,  $r_d$  the droplet radius,  $T_{air}$  the air temperature and  $Y_{v,air}$  the water vapor mass fraction in the air.

P. W Longest and M. Hindle, Numerical model to characterize the size increase of combination drug and hygroscopic excipient nanoparticle aerosols (2011).

## An Aerosol-fluid model with radius growth

We keep the same Navier-Stokes equation for the velocity field and add to the density function *f* the radius variable  $r \in \mathbb{R}^+$ . The new Vlasov-type equation writes :

$$\partial_t f + \mathbf{v} \cdot \nabla_x f + \operatorname{div}_{\mathbf{v}}(\alpha(\mathbf{u} - \mathbf{v})f) + \nabla_r(\mathbf{a}(\mathbf{r}, \mathbf{Y}_{\mathbf{v}, \operatorname{air}})f) = \mathbf{0}.$$

We complete by considering an advection diffusion equation for the evolution of water vapor mass fraction  $Y_{v,air}$ :

$$\partial_t Y_{v,air} + (u \cdot \nabla) Y_{v,air} - D\Delta Y_{v,air} = S_y,$$

completed with the following boundary and initial conditions :

$$\left( \begin{array}{ccc} Y_{\text{v,air}} &=& Y_{\text{v,air,in}}, \text{ on } \Gamma^{\text{in}}, \\ Y_{\text{v,air}} &=& Y_{\text{v,wall}}, \text{ on } \Gamma^{\text{wall}}, \\ \frac{\partial}{\partial n} Y_{\text{v,air}} &=& 0, \text{ on } \Gamma^{\text{out}}, \\ Y_{\text{v,air}}(0,\cdot) &=& Y_{\text{v,air,0}}, \text{ on } \Omega. \end{array} \right.$$

# Definition of the source term $S_{y}$

#### Proposition

Under the assumption that u = 0,  $\nabla Y_{v,air} = 0$  on  $\partial \Omega$  and

$$S_{y}(t,x) = -\frac{\rho_{w}}{\rho_{air}} \int_{\mathbb{R}^{3} \times \mathbb{R}^{+}} 4\pi r^{2} a(r, Y_{v,air}) f(t, x, v, r) dv dr,$$

the mass conservation is satisfied :

$$\frac{d}{dt}\left(\int \frac{4}{3}\pi\rho_{w}r^{3}\textit{fdxdvdr} + \int \rho_{\textit{air}}Y_{\textit{v,air}}dx\right) = 0, \ \forall t \geq 0.$$

#### Remark

The mass conservation is in accordance with the one satisfied by the ODE system.

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### Numerical scheme

For the fluid and water vapor mass fraction computation, we apply a finite element method on freefem. For the Vlasov equation we discretise the density *f* as a weighted sum of dirac masses :

$$f(t, x, v, r) \sim f^N(t, x, v, r) := \sum_{i=1}^{N_{\text{num}}} \omega_i \, \delta_{x_i(t), v_i(t), r_i(t)}(x, v, r),$$

where  $t \to (x_i(t), v_i(t))$  is the trajectory of the *i*<sup>th</sup> particle in the phase space and  $r_i(t)$  its radius. The number of initial particles  $N_{\text{Num}}$  is related to the physical aerosol particles  $N_{\text{Aero}}$  as follows :

$$N_{\text{Aero}} = \sum_{i=1}^{N_{\text{num}}} \omega_i.$$

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# Scheme algorithm

### Iteration loop on $n \ge 0$

- Computation of u<sup>n</sup> with retroaction source term coming from the previous time step.
- **2** Computation of  $Y_{v,air}^n$  using  $u^n$  and the source term coming from the previous time step.

### Local time loop for particles on $\tilde{n} \ge 0$

- Incrementation of the radius  $r_i^{\tilde{n}}$  for the *i*<sup>th</sup> particle (RK4).
- Computation of the velocity  $v_i^{\tilde{n}}$  (implicit scheme).
- Computation of the position  $x_i^{\tilde{n}}$  (explicit scheme).

Implementing the ODE model on Scilab and the aerosol-fluid model on Freefem we get :



here  $\Omega$  is a tube, the diffusion and the fluid velocity *u* are equal to 0.

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Image: Image:

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# Addition of temperature variation

Keeping the same Navier-Stokes equation we add to the density function f the droplet temperature  $T \in \mathbb{R}$ . The new Vlasov-type equation writes :

$$\partial_t f + \mathbf{v} \cdot \nabla_x f + \operatorname{div}_{\mathbf{v}}(\alpha(u - \mathbf{v})f) + \nabla_r(\mathbf{a}(r, T, Y_{v, air})f) + \nabla_T(\mathbf{b}(r, T, T_{air}, Y_{v, air})f) = 0,$$

We complete by considering an advection diffusion equation for the air temperature  $T_{\rm air}$ :

$$ho_{\mathsf{air}} \mathcal{C} \mathcal{P}_{\mathsf{air}} [\partial_t \mathcal{T}_{\mathsf{air}} + (u \cdot \nabla) \mathcal{T}_{\mathsf{air}}] - \mathcal{K}_{\mathsf{air}} \Delta \mathcal{T}_{\mathsf{air}} = \mathcal{S}_{\mathcal{T}}, \ \ \mathsf{on} \ \mathbb{R}^+ imes \Omega,$$

completed with the following boundary and initial conditions :

$$\begin{array}{rcl} T_{\rm air} &=& T_{\rm air,in}, \mbox{ on } \Gamma^{\rm in}, \\ T_{\rm air} &=& T_{\rm wall}, \mbox{ on } \Gamma^{\rm wall}, \\ \frac{\partial}{\partial n} T_{\rm air} &=& 0, \mbox{ on } \Gamma^{\rm out}, \\ T_{\rm air}(0, \cdot) &=& T_{\rm air,0}, \mbox{ on } \Omega. \end{array}$$

# Definition of the source term $S_T$

#### Proposition

Under the assumption that  $\nabla T_{air} = 0$ , u = 0 on  $\partial \Omega$  and

$$S_{T}(t,x) = \int [4\pi \rho_{w} r^{2} L_{v} a(r,T,Y_{v,air}) - mC \rho_{d} b(r,T,T_{air},Y_{v,air})] f dv dr dT,$$

the thermal energy balance writes :

$$\begin{split} \rho_{air} C p_{air} \int \partial_t T_{air} dx + C p_d \int m b(r, T, T_{air}, Y_{v,air}) f dx dv dr dT = \\ \int 4 \pi L_v r^2 \rho_w a(r, T, Y_{v,air}) f dx dv dr dT. \end{split}$$

#### Remark

The thermal energy balance is in accordance with the one satisfied by the ODE system.

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#### Particle position comparison with/without temperature variation



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#### Radii comparison with/without temperature variation



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#### Y<sub>v,air</sub> comparison with/without temperature variation



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# Conclusion and prospects

### Conclusion

- The radius growth rate is between 2 and 10.
- Including temperature variation in the model decreases the radius growth rate.

#### Prospects

- 3D implementation.
- Considering a multiple bifurcation tree.
- Existence and uniqueness of the coupled problem.
- Numerical tests on the aerosol deposition maps.

# Thank you for your attention

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